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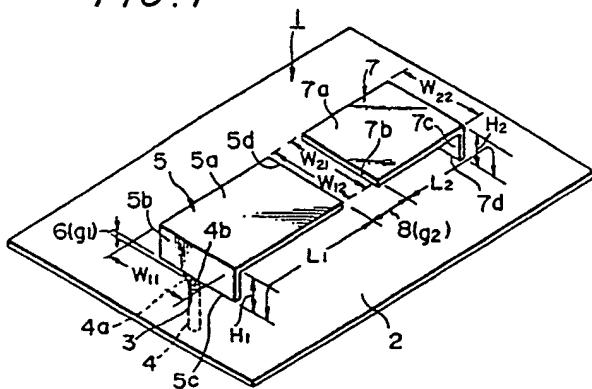
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(54) Wide band antenna for mobile communications.

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(57) In order to provide an increased resonant band width for an antenna device for vehicles on a ground plate (2) having a flat surface a L-shaped radiator plate (5) is attached having one leg (5a) of L arranged parallel to said ground plate (2) with the other leg (5b) being positioned perpendicular to said ground plate (2), said radiator plate being disposed having a narrow gap (6g1) between the lower end (5c) of said vertical leg (5b) and the upper surface of said ground plate; further a sub-radiator element (7) formed by a L-shaped plate is rigidly mounted on said ground plate (2) at a position in close proximity to said radiator plate (5) the free ends (5d, 7b) of said radiator plate (5) and of said sub-radiator element (7) having a given distance (8g2).

FIG. 1



WIDE BAND ANTENNA FOR MOBILE COMMUNICATIONS

Background of the Invention

Field of the Invention:

The present invention relates to an antenna to be mounted on a travelling equipment such as vehicle or the like.

Description of the Prior Art:

The recent development of tele-communication technology has significantly promoted the progressive applications in the fields of wire communication and especially radio communication.

In mobile radio communication systems being able to perform the simultaneous transmission and reception of information signals such as a duplex communication system in land mobile radio-telephones and the like, the signals are modulated by the use of carriers having different frequencies, respectively. The frequencies of the respective carriers for sending and returning signals must be separated away from each other sufficiently to prevent the interference between two carriers.

Consequently, an antenna mounted on a vehicle must have its sufficiently widened resonant frequency band to contain said two different frequencies for transmission and reception, and it must be small and low profile.

In the prior art, the small antenna on the vehicle is frequently in the form of inverted F antenna shown in Figure 11, which comprises an L-shaped radiator plate 5 having one leg connected electrically and mechanically with a ground plate 2. To take the proper impedance matching, the antenna is fed at a point which is slightly spaced away from the bent portion of the L-shaped radiator (offset feed).

Such an antenna has only its very narrow band width which is in the order of a few percent of the carrier frequency. Due to any external factor, thus, the resonant frequency of the antenna would be frequently shifted to be forced out of the frequency bands covering the transmission and reception frequencies, resulting in interrupted transmission or reception.

Some attempts have been made to overcome the above disadvantages in the prior art. One of these attempts is that an antenna includes an auxiliary plate (sub-radiator) 11 positioned in parallel to the radiator 5, as shown in Figure 12. The sub-radiator plate 11 is non-feed driven. Another at-

tempt is that an additional plate 7 is positioned adjacent to the radiator 5, as shown in Figure 13. These improvements are intended to overlap the resonant frequency bands produced by both the radiator and the sub-radiator to provide a more widened resonant frequency band such that it will not be forced away from the transmission and reception frequency band due to any external factor.

A further attempt has been made that an antenna includes an impedance compensating element 12 additionally connected with the feed line of the antenna to increase the resonant frequency band width such that the impedance matching with the feed line is provided (Figure 14).

However, within the resonant frequency band in the prior antenna, a range in which a return loss is less than a predetermined voltage standing wave ratio ($VSWR < 2.0$), that is, a range in which the return loss is less than -10db could not be expected over 7% - 9% in the fractional band (Figure 15). Thus, it was not believed that the prior art can provide any improved antenna system having an increased degree of freedom with which the resonant frequency band is sufficiently widened.

In particular, the two way simultaneous transmission and reception system for automobiles, which is intended by the present invention, has an antenna surrounded by various automobile components by which the transmission and reception of the antenna would be adversely affected. It is therefore desired to provide a radio communication antenna which has a widened band width with a degree of freedom for stabilizing the transmission and reception even under the above circumstances.

SUMMARY OF THE INVENTION

It is therefore an object of the present invention to provide a wide band antenna system for mobile communications, in which a dual resonant created by a radiator and a sub-radiator is utilized to provide an increased and stabilized resonant frequency band such that the transmission and reception can be performed more freely and to provide such an antenna system which is reduced in size sufficiently to be mounted on an automobile and can be manufactured more easily.

To this end, the present invention provides a wide band antenna system for mobile communications, comprising a ground plate having a flat surface, an L-shaped radiator plate having one leg of L

arranged parallel to said ground plate with the other leg being positioned perpendicular to said ground plate, said radiator plate being disposed having a gap between the lower end of said vertical leg and the upper surface of said ground plate, a coaxial feed cable for connecting said ground plate with an outer conductor and also for connecting an inner conductor with substantially the center of said vertical leg end of said radiator plate, and an additional conductive no-feed element (sub-radiator) formed by an L-shaped plate rigidly mounted on said ground plate at a position in close proximity to said radiator plate, said sub-radiator having one leg extending parallel to said ground plate with the end thereof being spaced away from the end of the parallel leg of said radiator plate by a given distance, the vertical leg of said L-shaped plate having the end connected with said ground plate to provide an increased band width.

In such an arrangement, the opened end of the radiator plate is located opposite to that of the sub-radiator with a given spacing therebetween. This is intended to utilize the variations of a feed point impedance due to a current induced in the sub-radiator to provide a very widened frequency band in which the real part of the impedance can be maintained, at the same value as or a value very near to the impedance of the feed line (normally equal to 50 Ohms) under a resonant condition (or when the imaginary part of the impedance is equal zero).

In the antenna system of the present invention, there is further a given gap between the lower end of the radiator plate connected with feed line and the upper surface of the ground plate. Such a gap provides a capacitance functioning to offset a reactance component corresponding to the imaginary part of the impedance of the antenna. When this gap was properly regulated, the imaginary part of the impedance could be maintained substantially at zero or a value substantially equal to zero over the widened frequency band width.

Figure 2 shows the relationship between the real and imaginary parts of the feed point impedance of the antenna, relative to a frequency used by the aforementioned antenna system which is constructed according to the present invention. As seen from Figure 2, the frequency band matching the impedance of the feed line (50 Ohms), that is, the resonant frequency band can be increased sufficiently.

In accordance with the present invention, the antenna system can have a widened frequency band (resonant frequency band) in which the sufficient number of different frequency bands can be included, since the antenna system comprises a radiator plate having its opened end opposed to the opened end of a sub-radiator element, the

impedance of the feed point being regulated to create a dual resonance by the use of a current induced in the sub-radiator element. Accordingly, the transmission and reception can be carried out satisfactorily even though the antenna is adversely affected to shift the resonant frequency band by any external factor.

Thus, the antenna system of the present invention could have a fractional resonant frequency band width of 30% or higher which could match the impedance in the feed line.

Furthermore, the antenna system is of a very simplified construction and can easily realize a matching in a desired frequency band by modifying the size and shape of the antenna.

Therefore, the antenna system may be applied to various applications and is optimum for a transmitter and receiver antenna which is to be mounted on any vehicle such as automobile or the like.

Furthermore, the antenna system of the present invention can be reduced in size. In other words, the entire antenna system can be reduced in size by the fact that a dielectric material is interposed between the radiator plate and the ground plate and between the sub-radiator element and the ground plate. Where the relative dielectric constant of the dielectric material used in the antenna system of the present invention is ϵ_r , the shortening coefficient of wave-length is approximately represented by

$$1/\sqrt{\epsilon_r}$$

This means that the effective resonant length of the antenna can be shortened by using a dielectric material having its increased relative dielectric constant.

The present invention preferably uses a material having its increased relative dielectric constant such as epoxy resin, Teflon, glass or the like.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic view showing the first embodiment of the present invention.

Figure 2 is a graph showing the variations of real and imaginary parts of the antenna feed point impedance relative to various frequencies.

Figure 3 is a graph showing the return loss characteristic of the antenna in the first embodiment of the present invention.

Figure 4 is a graph showing the return loss characteristic of the antenna in the second embodiment of the present invention.

Figure 5 is a schematic view of the third embodiment of the present invention.

Figure 6 is a schematic view of the fourth embodiment of the present invention in which a radiator plate is supported by a supporter relative to a ground plate.

Figure 7 is a cross-sectional view of the fifth embodiment of the present invention in which a radiator plate is spaced away from a ground plate by a given gap and rigidly supported on the ground plate by means of a molding resin.

Figure 8 is a schematic view of the sixth embodiment of the present invention in which a radiator plate and a sub-radiator element are molded by a supporter having sloping outer wall faces.

Figure 9 is a cross-sectional view of the sixth embodiment shown in the Fig. 8.

Figure 10 is a schematic view of the seventh embodiment of the present invention in which a sub-radiator element is electrically connected with a ground plate through a narrow bridge portion.

Figures 11, 12, 13 and 14 are schematic views showing various antenna configurations in the prior art.

Figure 15 is a graph showing the variations of return loss relative to various frequencies in an antenna system constructed according to the prior art.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring now to Figure 1, there is shown an antenna 1 for vehicles, which is adapted to be mounted on an automobile body and to perform the transmission and reception of radio waves between the automobile and a radio base station.

The antenna 1 comprises a ground plate 2 formed of a flat conductive plate. The ground plate 2 includes an opening 3 formed therethrough. The opening 3 receives an inner conductor (core wire) 4b of a coaxial feed cable 4 without electrical connection while the inner edge of the opening 3 is electrically connected with an outer conductor 4a of the coaxial cable 4.

On the ground plate 2 is placed a radiator plate 5. The radiator plate 5 is formed of an L-shaped conductive plate with one leg 5a being positioned parallel to the ground plate 2. The other or vertical leg 5b of the radiator plate 5 has one edge 5c spaced apart from the ground plate 2 by a given narrow gap 6 (g_1). The edge 5c of the radiator plate 5 is electrically connected substantially at its center with the inner conductor 4b of the coaxial feed cable 4.

In order to provide a widened band, a sub-radiator element 7 formed of an L-shaped conductive plate is mounted on the ground plate in prox-

imity to the radiator plate 5 with one leg 7a being positioned parallel to the ground plate 2. The one leg 7a of the sub-radiator element 7 is located opposed to the end 5d of the radiator plate 5 with a given gap 8 (g_2) therebetween. The other or vertical leg 7c of the sub-radiator element 7 has one end 7d connected with the ground plate 2.

The length L_1 of the radiator plate 5 measured from the feed end 4b of the coaxial cable 4 to the end 5d of the radiator plate 5 is set to be slightly larger than one-fourth the wave-length λ used herein while the length L_2 of the sub-radiator element 7 is selected to be slightly smaller than one-fourth the wave-length λ used herein.

Various dimensions of an automobile antenna system designed for 1 G Hz band in accordance with the principle of the present invention are as follows:

Length of radiator plate $L_1 = 70$ mm;
 $W_{11} = W_{12} = 50$ mm;
 $H_1 = 20$ mm;
 $g_1 = 1$ mm;
 $L_2 = 45$ mm;
 $W_{21} = W_{22} = 50$ mm;
 $H_2 = 20$ mm; and
 $g_2 = 22$ mm.

The antenna having the aforementioned dimensions has return loss characteristics shown in Figure 3.

From this figure, it can be seen that the fractional resonant band exceeds 20% in the first embodiment of the present invention. In this connection, the fractional resonant band could be increased to 40% if the heights H_1 and H_2 of the radiator and sub-radiator plates were increased up to 30 mm respectively.

In the second embodiment, a further increased band width can be realized by regulating the widths W_{11} , W_{12} ; W_{21} , W_{22} of the radiator and sub-radiator plates in the antenna system.

The dimensions of the second embodiment used to obtain the above advantage is as follows:

Width of radiator plate $W_{11} = 50$ mm;
 $W_{12} = 20$ mm;
 $g_2 = 12$ mm; and
 g_1 Other dimensions being the same as those of the first embodiment.

The antenna system having the above dimensions has return loss characteristics shown in Figure 4. It can be seen from this figure that the fractional resonant band becomes 30% or more.

In such a manner, the first and second embodiments of the present invention can provide an antenna system having an increased degree of free-

dom which provide a widened frequency band width (resonant frequency and width) by modifying the size and shape of the antenna.

Referring now to Figure 5, there is shown in the third embodiment providing an antenna system 1 which is further reduced in size and has an increased mechanical strength.

In the third embodiment, fillers each formed of a dielectric material having its good high-frequency characteristics, such as Teflon, epoxy resin, glass or the like are interposed between the ground plate 2 and the radiator plate 5 and between the ground plate 2 and the sub-radiator element 7. In such a case, the Teflon fillers 9 have their relative dielectric constant $\epsilon_r = 2.6$. Thus, the size of the entire antenna could be reduced up to about 20%. Further, the interposition of the fillers 9 permits the antenna system to withstand vibrations from the vehicle on which it is mounted.

Figure 6 shows the fourth embodiment of the present invention having a structure similar to that of the first embodiment shown in Figure 1, wherein an L-shaped radiator plate 5 is floated above a ground plate 2 with a gap 6 (g_1) formed therebetween.

In the fourth embodiment, the radiator plate 5 has one leg 5a placed on a supporter 20 parallel to the ground plate 2. Such an arrangement supports the radiator plate 5 above the ground plate 2 while maintaining the gap 6 (g_1) properly.

The supporter 20 is preferably made of any suitable electrically insulating material such as foamed styrene or the like.

Figure 7 shows the fifth embodiment of the present invention in which an antenna system 1 is mounted within a casing. The casing comprises a base plate 21 and a closure 22, both of which are made of any suitable electrically insulating material such as plastic material or the like.

A ground plate 2 is rigidly mounted on the base plate 21 by any suitable joining means such as adhesion or the like.

The base plate 21 also rigidly supports a coaxial cable 4 by clip means such that the coaxial cable 4 is introduced into the casing. The coaxial cable 4 includes an outer conductor 4a joined to the ground plate 2 and an inner conductor 4b connected with the vertical leg 5b of an L-shaped radiator plate 5 at its edge.

As seen from Figure 7, an L-shaped sub-radiator element 7 has its vertical leg 7c rigidly connected at one end with the ground plate 2 by any suitable joining means such as welding or the like. On the other hand, a molding resin 24 is charged into the casing such that the radiator plate 5 is rigidly mounted on the ground plate 2 with a gap 6 (g_1) formed therebetween. The molding resin is preferably of foamed styrene or Teflon.

In the fifth embodiment, the radiator plate 5 can be properly positioned relative to the ground plate 2 with the gap formed therebetween, by the use of the molding resin.

Figures 8 and 9 show the sixth embodiment of the present invention in which an L-shaped radiator plate 5 and a similar L-shaped sub-radiator element 7 are supported on a ground plate 2 by means of fillers 9 and further covered by supporter 20 having the shape of a frustum of a pyramid.

In the embodiment, the fillers are made of dielectric material which has good high-frequency characteristics. Teflon, epoxy resin or glass are preferable to provide such dielectric material. Molded resin is interposed between the ground plate 2 and the radiator plate 5 to make a slightly narrow channel therebetween for supporting the radiator plate 5 in separated disposition above the ground plate 2. On the other hand, the sub-radiator element 7 is rigidly mounted on the ground plate 2 with the parallel leg thereof being opposed to the parallel leg of the radiator plate 5. The spaced room between the sub-radiator 7 and the ground plate 2 is then filled with molded resin for increasing the dielectric constant of the sub-radiator.

The antenna of the embodiment is further molded by supporter 20 being made of foamed styrene for example to solidify the shape of the antenna. Molding the supporter 20 provides the external shape of a frustum of a pyramid to the antenna in which the upper surfaces of the radiator plate 5 and the sub-radiator element 7 are exposed outwardly. Such a frustum of a pyramid shaped supporter 20 can protect the antenna from collision or mechanical shock. As shown in figures the molding supporter 20 can cover the radiator plate 5 and the sub-radiator element 7 except their upper surfaces for securely mounting the plate 5 and the element 7 on the ground plate 2. According to the shape of a frustum of a pyramid, the supporter 20 has sloping outer wall faces on its four sides so as to provide the rounding off shape on the outer surface thereof. The above mentioned shape is preferable to realize a well-formed design for an antenna equipment being placed on the back seat tray of the automobiles.

Figure 10 shows the seventh embodiment of the present invention which is similar to the third embodiment shown in Fig. 5. In contrast to the third embodiment, the sub-radiator element 7 of the present embodiment has a connecting bridge portion 7e for making an electrical conductivity between the sub-radiator 7 and the ground plate 2 within a restricted narrow path. Accordingly the remainder of the end portion 7d of the sub-radiator element 7 is kept in electrically insulated relation to the ground plate 2. The bridge portion 7e is preferably provided on one side of the vertical leg 7c of

the sub-radiator element 7.

By restricting the electrical conductivity path between the element 7 and the ground plate 2, induced electric current in the element 7 on receiving radio waves will make a plurality of current pathes shown l_1 - l_4 in Fig. 10 since the end of the pathes is closed tight to the connecting bridge portion 7e. The length of each path is therefore different from the other, for instance, path l_4 is larger than path l_3 and so on. As well known in the art, the length of the induced current path will define the wavelength of the received radio signals, therefore, the different length of the pathes can widen the resonant frequency of the sub-radiator 7. Accordingly, the seventh embodiment shown in Fig. 10 can provide an antenna having a widened resonant band width.

Although the bridge portion 7e of the shown embodiment is composed in the projected portion from the vertical leg 7c of the element 7, the bridge of this invention can be formed by a solder conductivity path, a lead wire or the like.

Claims

1. An antenna device (1) for vehicles, comprising a ground plate (2) having a flat surface, a L-shaped radiator plate (5) having one leg (5a) of L arranged parallel to said ground plate (2) with the other leg (5b) being positioned perpendicular to said ground plate (2), said radiator plate being disposed having a narrow gap (6g1) between the lower end (5c) of said vertical leg (5b) and the upper surface of said ground plate, a feed coaxial cable (4) for connecting said ground plate with an outer conductor (4a) and also for connecting an inner conductor (4b) with substantially the center of said vertical leg end (5c) of said radiator plate, and a sub-radiator element (7) formed by a L-shaped plate rigidly mounted on said ground plate (2) at a position in close proximity to said radiator plate (5), said sub-radiator element (7) having one leg (7a) extending parallel to said ground plate (2) with the end (7b) thereof being spaced away from the end (5d) of the parallel leg (5a) of said radiator plate (5) by a given distance (8g2), the vertical leg (7c) of said L-shaped plate (7) having the end (7d) connected with said ground plate (2) to provide an increased resonant band width.

2. An antenna device as defined in claim 1, further comprising filler means (24) for surrounding said ground plate (2), said radiator plate (5) and said sub-radiator element (7), said filler means being made of dielectric material which has good high-frequency characteristics.

3. An antenna device as defined in claim 1, wherein filler means (9, 24) at least interposed between the ground plate (2) and the radiator plate (5) and between the ground plate (2) and the sub-radiator element (7).

4. An antenna device as defined in claim 3 wherein said filler means is made of one selected from Teflon, epoxy resin or glass.

5. An antenna device as defined in claim 3, further comprising support means (20) covering the part of the outer surfaces of said radiator plate (5) and said sub-radiator element (7) for rigidly mounting said radiator plate and said sub-radiator plate on said ground plate (2).

10 6. An antenna device as defined in claim 5, the outer surface of said support means (20) has sloping outer wall faces for rounding off the outer surface thereof.

7. An antenna device as defined in claim 1, further comprising support means (20, 24) for rigidly mounting said radiator plate (5) on said ground plate (2) with the end of the vertical leg (5b) of said radiator plate (5) being floated above said ground plate (2) by a given narrow gap (6g1) therebetween, said support means being made of an electrically insulating material.

20 8. An antenna device as defined in claim 6 or 7, wherein said support means is made of foamed styrene.

9. An antenna device as defined in claim 7, wherein said support means (24) includes a molding resin which is set to surround said radiator plate (5) and said sub-radiator element (7) with said radiator plate (5) being spaced away from said ground plate by said given narrow gap (6g1).

30 10. An antenna device as defined in any of claims 1 to 9, wherein the length (L_1) of said radiator plate (5) is set to be slightly larger than one-fourth the wave-length λ of a carrier and wherein the length (L_2) of said sub-radiator element (7) is set to be slightly smaller than one-fourth the wave-length λ of the carrier.

11. An antenna device for vehicles, comprising a ground plate (2) having a flat surface, a L-shaped radiator plate (5) having one leg (5a) of L arranged parallel to said ground plate (2) with the other leg (5b) being positioned perpendicular to said ground plate (2), said radiator plate being disposed having a narrow gap (6g1) between the lower end (5c) of said vertical leg (5b) and the upper surface of said ground plate, a feed coaxial cable (4) for connecting said ground plate with an outer conductor (4a) and also for connecting an inner conductor (4b) with substantially the center of said vertical leg end (5c) of said radiator plate, and a sub-radiator element (7) formed by a L-shaped plate being disposed close to said ground plate (2) at a position in opposite proximity to said radiator plate (5), said

sub-radiator element (7) having one leg (7a) extending parallel to said ground plate (2) with the end (7b) thereof being spaced away from the end (5d) of the parallel leg (5a) of said radiator plate (5) by a given distance (8g2), the vertical leg (7c) of said L-shaped plate (7) having a connecting bridge portion (7a) rigidly connected with said ground plate (2) at one side of the vertical leg to widen a resonant band width.

12. An antenna device as defined in claim 11, further comprising filler means (9) for surrounding said ground plate (2), said radiator plate (5) and said sub-radiator element (7), said filler means being made of dielectric material which has good high-frequency characteristics; wherein the length (L_1) of said radiator plate (5) is set to be slightly larger than one-fourth the wave-length λ of a carrier and wherein the length (L_2) of said sub-radiator element (7) is set to be slightly smaller than one-fourth the wave-length λ of the carrier.

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FIG. 1

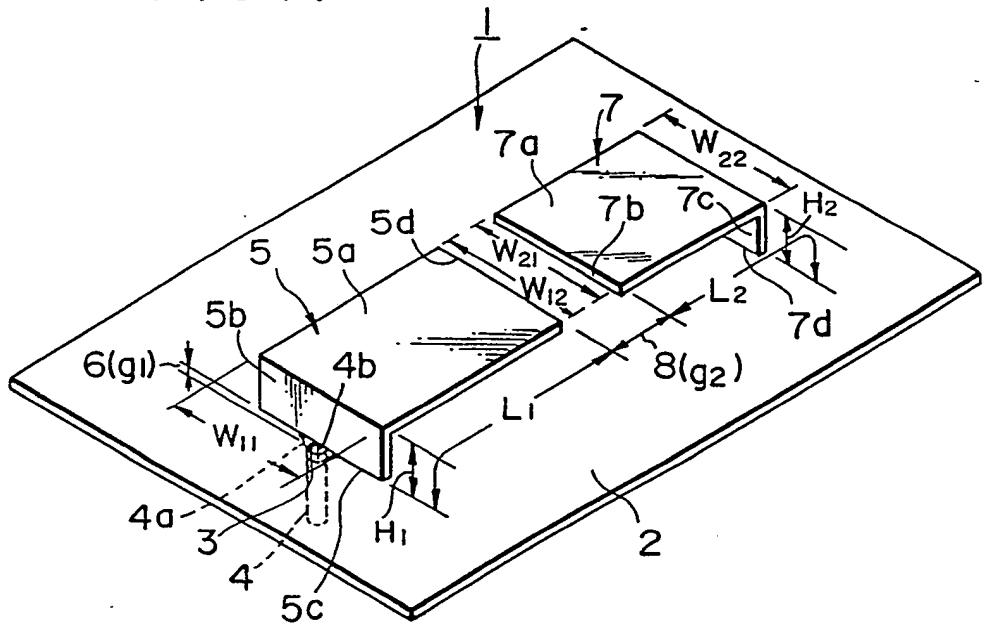


FIG. 2

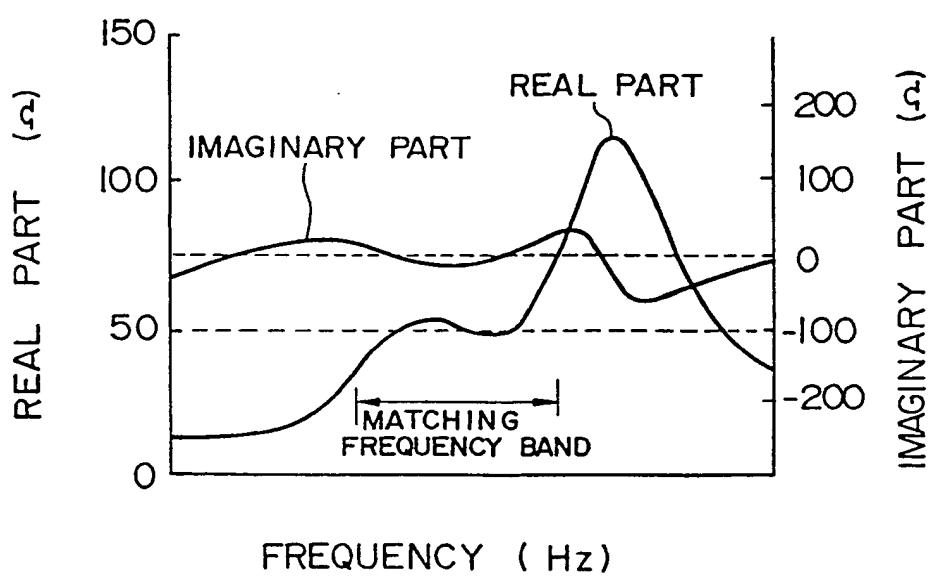


FIG. 3

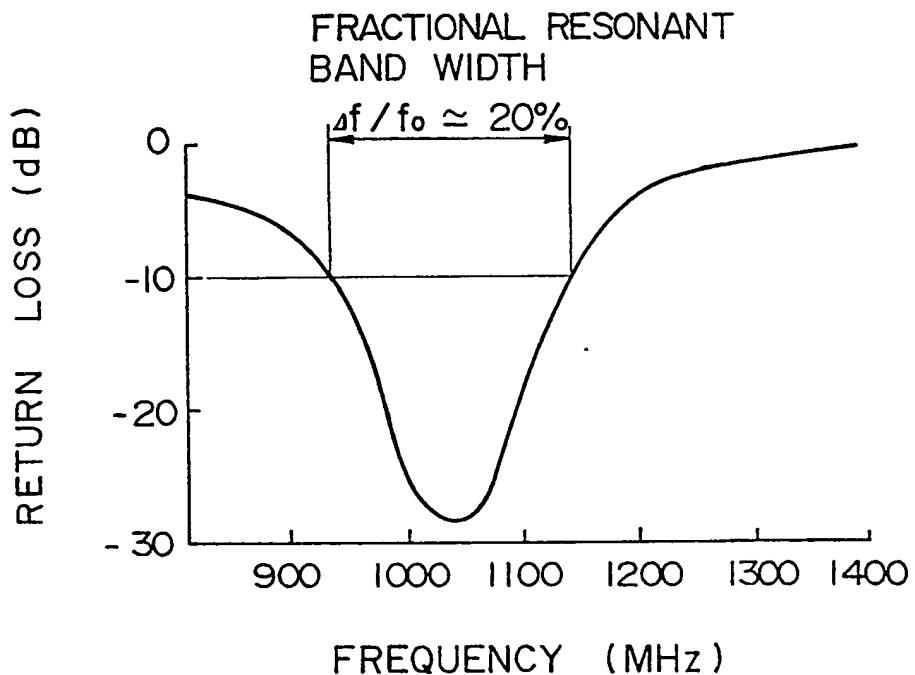


FIG. 4

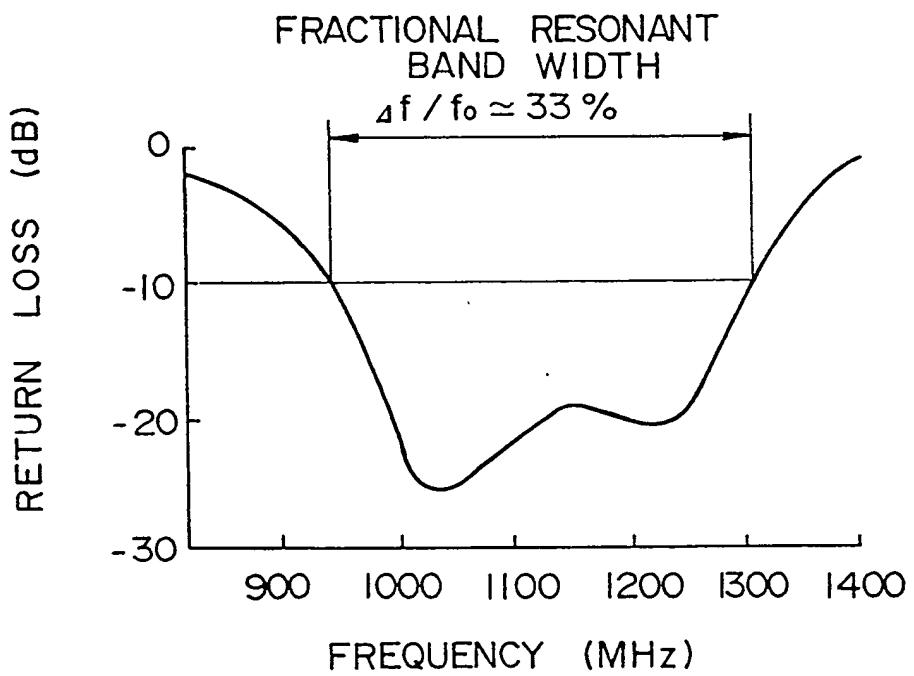


FIG. 5

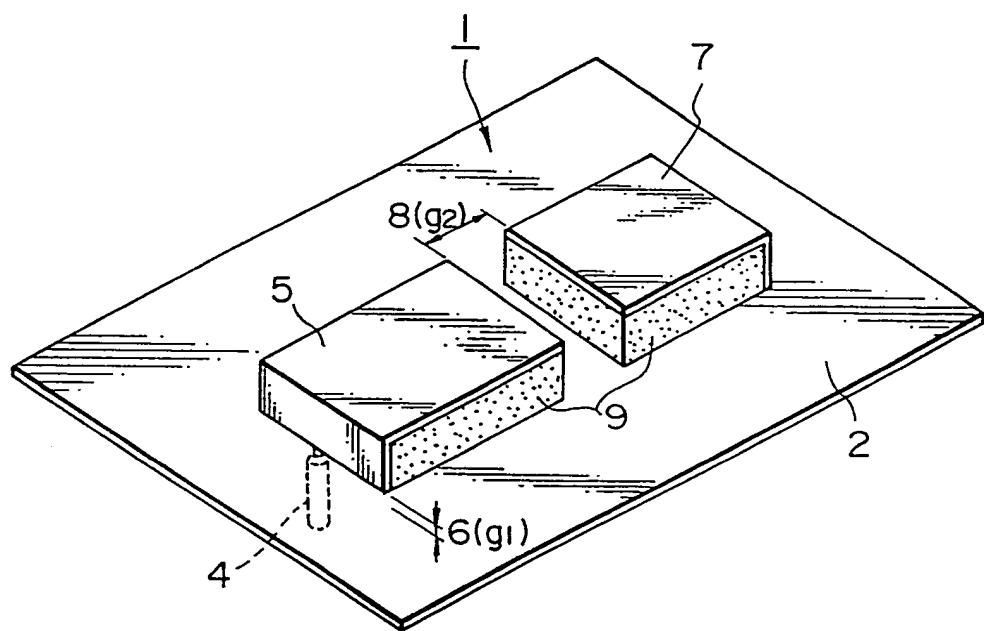


FIG. 6

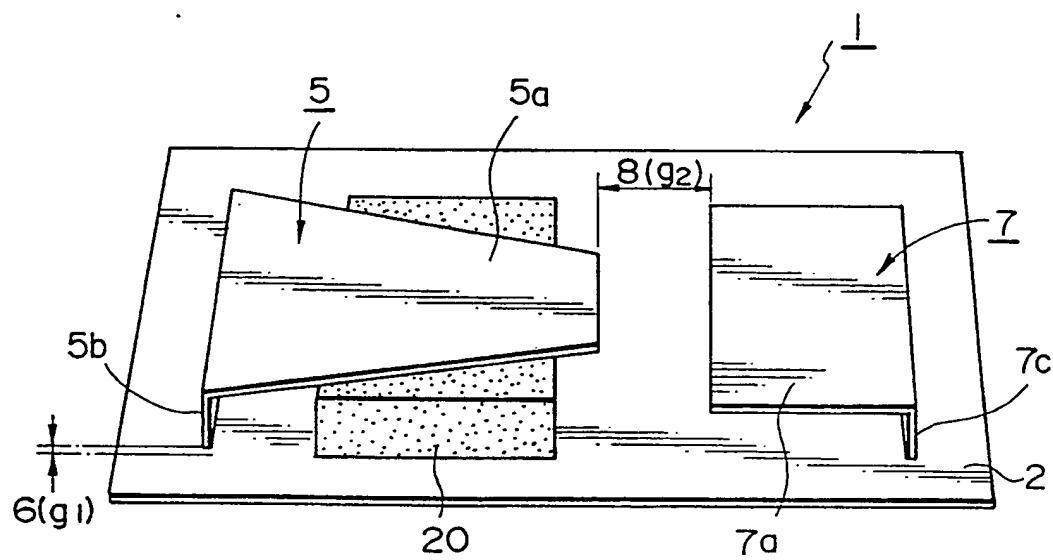


FIG. 7

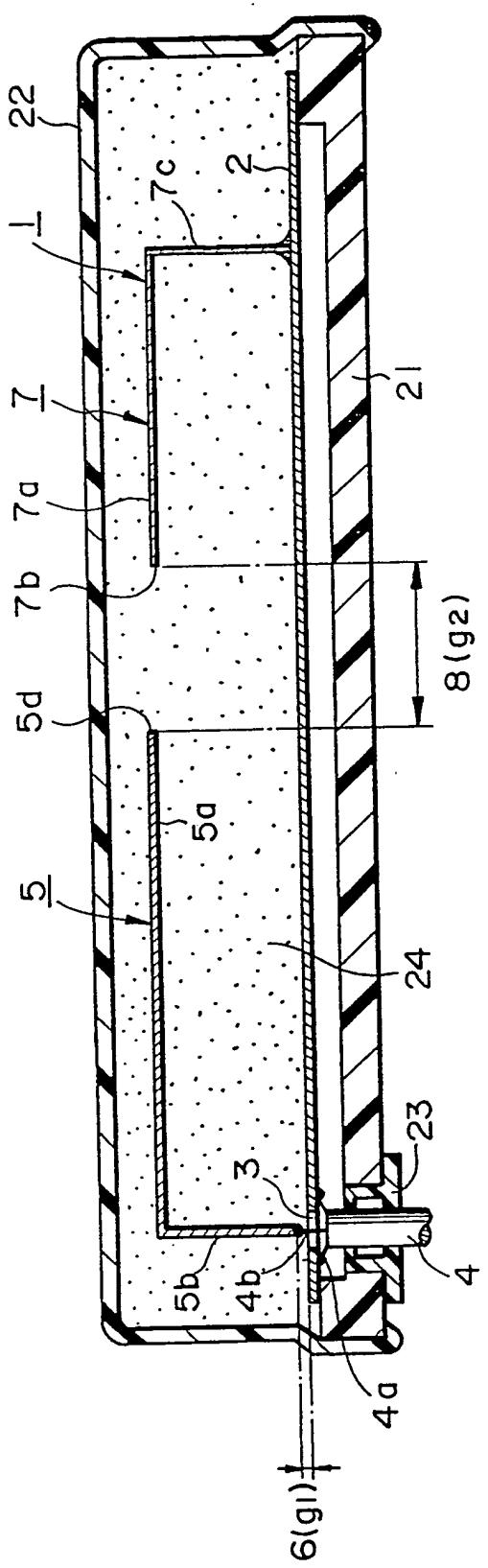


FIG. 8

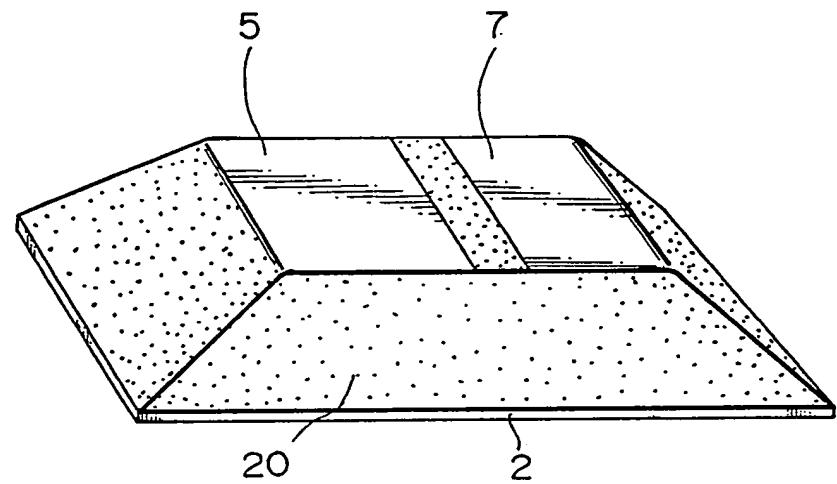
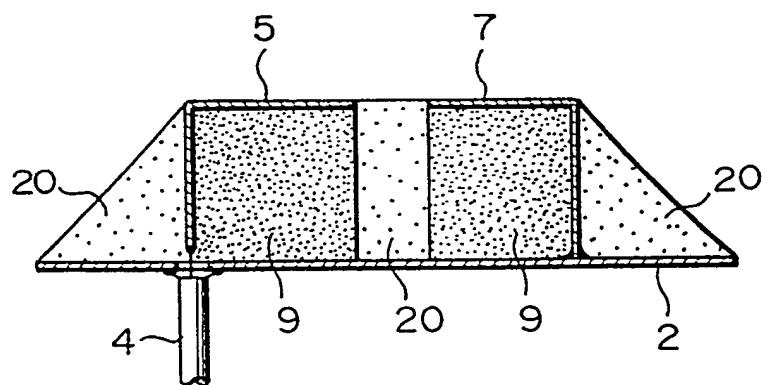


FIG. 9



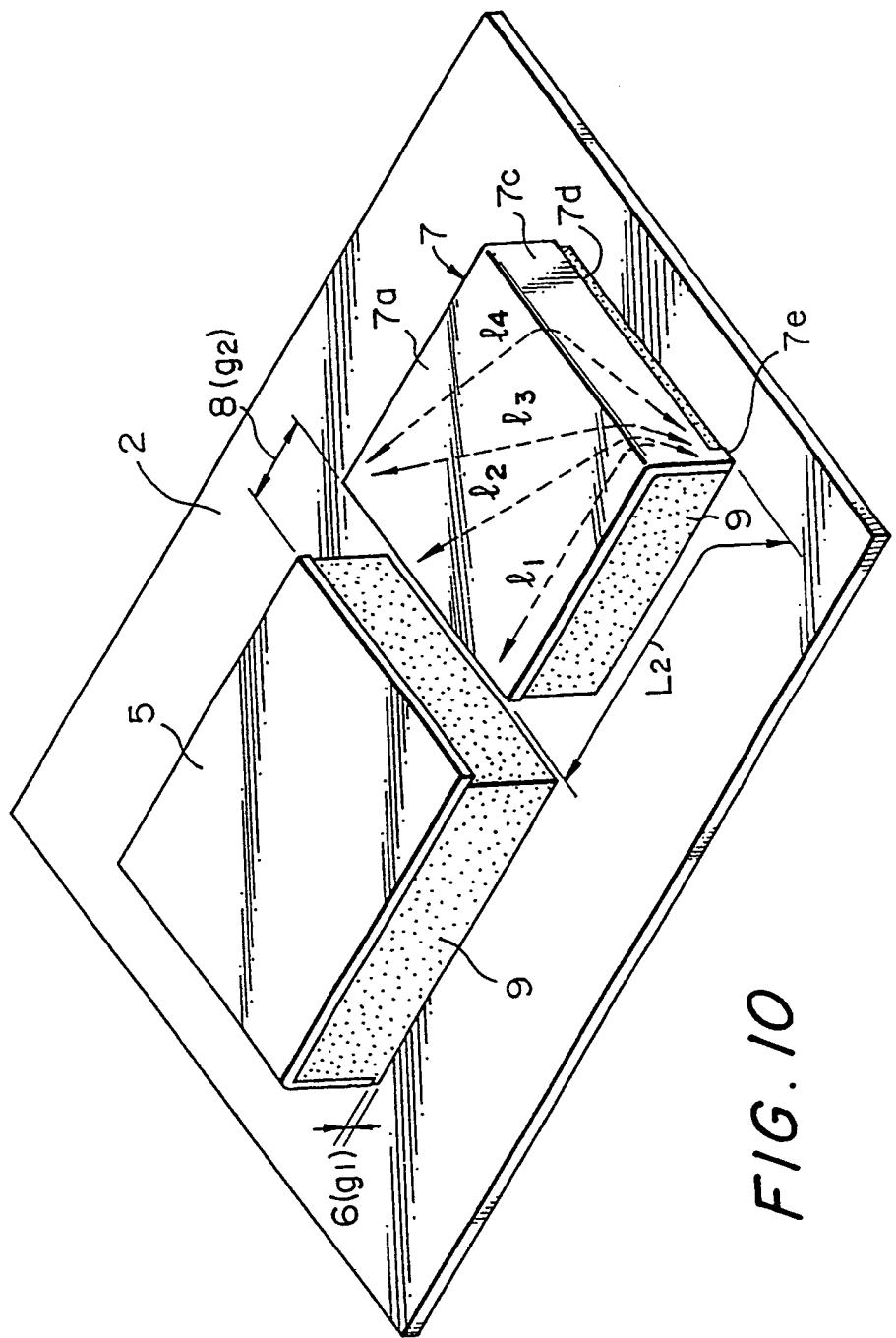


FIG. 10

FIG. 11

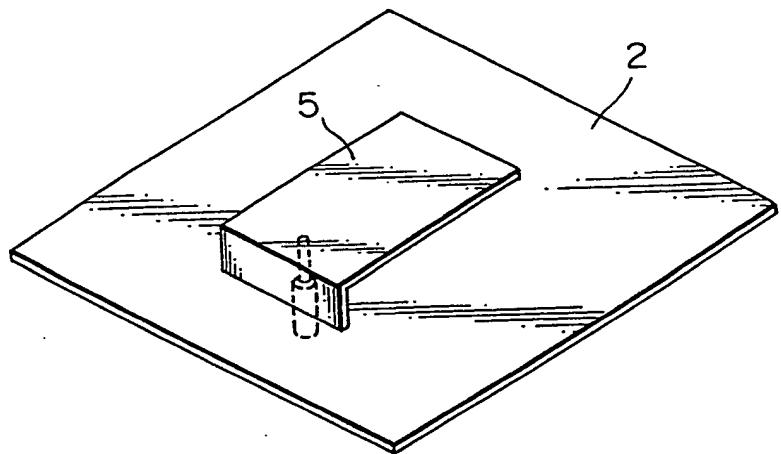


FIG. 12

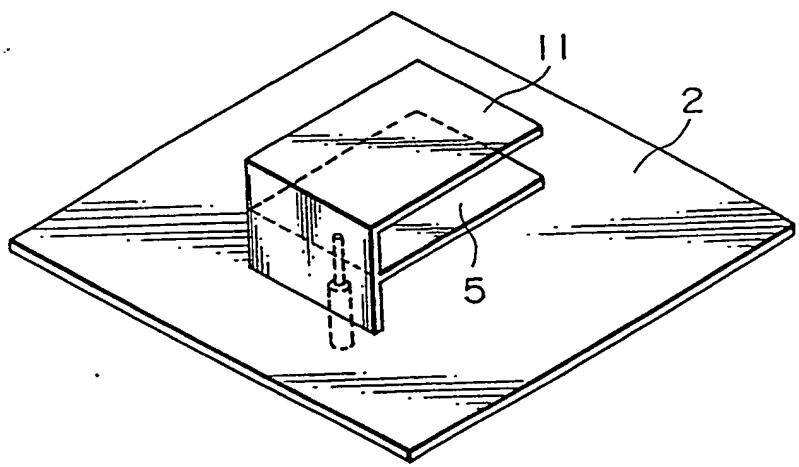


FIG. 13

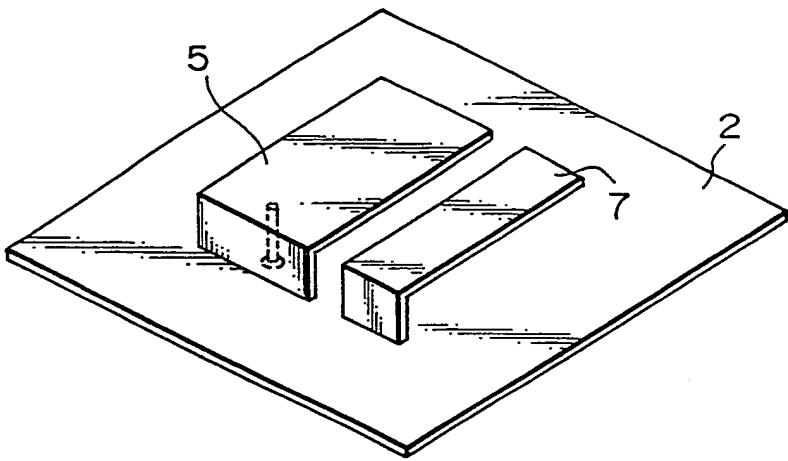
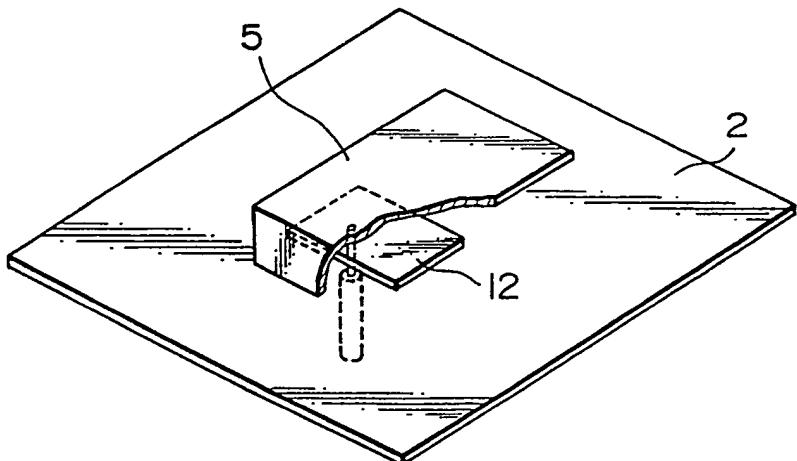


FIG. 14



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FIG. 15

